

The Cooper Union
Department of Electrical Engineering
ECE135 Engineering Electromagnetics
Exam III
May 7, 2012

Time: 3 hours. Closed book, closed notes. Calculator provided.

Part I: Maxwell's Equations and Constitutive Relations. 20pts. total.

1. State Maxwell's equations in **differential** form for the following cases:
 - (a) In the time-domain, in the most general case.
 - (b) In the phasor domain, assuming a linear homogenous isotropic lossy medium (σ, μ, ϵ) , but $\rho = 0$.
2. Write the general relation among $\vec{D}, \vec{E}, \vec{P}$ and give units for all quantities that appear.
3. Write the general relation among $\vec{B}, \vec{H}, \vec{M}$ and give units for all quantities that appear.

Part II: Answer all problems.

1. [2 pts.] Short answers:

- (a) An infinitesimal dipole antenna is called a _____ dipole.
- (b) True or false: The current distribution on a straight-wire antenna is tapered to 0 at the endpoints.

2. [4 p.ts] When $2A$ is applied to a lossless antenna, $100W$ of power is radiated. You have enough information to determine an antenna parameter. Name it, and compute its value.

3. [6 pts.] Consider an antenna with radiation pattern $K(\theta, \phi)$, and total radiated power W .

- (a) What are the units of K ?
- (b) Write a formula for the power density at a point (r, θ, ϕ) , in W/m^2 .
- (c) Write a formula for the directive gain $g_D(\theta, \phi)$.
- (d) Suppose this antenna is used in an array, with an array pattern with directivity $20dB$. If you know g_D for the elemental antenna, do you have information to determine the directivity of the array? If yes, what is it? If not, what more information would you need?

4. [6 pts.] The total field of the magnetic dipole antenna (loop of radius a centered at the origin in the xy -plane) is, in spherical coordinates:

$$\begin{aligned} E_\phi &= -\frac{j\omega\mu I a^2}{4} e^{-jkr} \left(\frac{jk}{r} + \frac{1}{r^2} \right) \sin\theta \\ H_r &= \frac{j\omega\mu I a^2}{4} e^{-jkr} \left(\frac{2}{\eta r^2} + \frac{2}{j\omega\mu r^3} \right) \cos\theta \\ H_\theta &= \frac{j\omega\mu I a^2}{4} e^{-jkr} \left(\frac{j\omega\varepsilon}{r} + \frac{1}{j\omega\mu r^3} + \frac{1}{\eta r^2} \right) \sin\theta \end{aligned}$$

and the other field components are zero.

- (a) Write the terms for the near-field approximation. Examine the near-field to determine: whether the power density is purely real, purely reactive, or a mix; the dependence of power with distance (i.e., $1/r^m$: what is m ?); whether there is a component of the (complex) Poynting vector that is NOT radial. *Do not compute the actual Poynting vector; do not invoke results you remember- show how your near-field approximation leads to the results.*
- (b) Write the terms for the far-field approximation. Then repeat part a above to describe the (complex) Poynting vector without actually computing it.

5. [2 pts.] Consider an aperture antenna modeled with equivalent sources \vec{J}_s (surface electric current) and \vec{M}_s (surface magnetic current). Pick the one that is NOT TRUE!! (One is false, the others are true).
- \vec{J}_s depends on \vec{H} tangential to the aperture;
 - \vec{M}_s depends on \vec{E} tangential to the aperture;
 - if we are interested in the far-field, there is no need to model the normal \vec{E} and \vec{H} components with equivalent sources;
 - the total \vec{E}, \vec{H} fields in the far-field are represented by the single vector potential \vec{A} .
6. [7 pts.] This question concerns guided waves in cylindrical waveguides. Short answer:
- Briefly define (one sentence or less): dominant mode.
 - Briefly define (one sentence or less): degenerate mode.
 - A single mode propagating in an “ideal” material can nevertheless experience dispersion. This type of dispersion is called _____ dispersion, and can be mitigated by operating at (*higher/lower*) frequencies.
 - The wave impedance for a mode will be purely reactive if operated (*above/below*) the cutoff frequency. This results in a(n) _____ wave.
 - True or False (no justification): When establishing the scattering parameter model, the “voltage” is computed as the integral of the \vec{E} -field in the cross section, and the “current” is computed as the integral of the surface current in the cross-section.
7. [4 pts.] For a TE or TM mode in a cylindrical closed boundary waveguide: Draw a sketch of the “universal curve” for ω versus β , and use this curve (NOT FORMULAS) to show that the group velocity (*increases/decreases*) (which?) as you increase frequency.
8. [4 pts.] Give the two main reasons many practical devices are realized by employing the TE_{10} mode in a rectangular waveguide. Such devices will be limited to operating within a certain frequency range; give the upper and lower frequencies (I don’t mean a formula; I mean identify these frequencies and WHY we are limited to operate between them: be BRIEF but clear).
9. [9 pts.] Given a $3\text{cm} \times 5\text{cm}$ rectangular waveguide filled with a dielectric with $\epsilon_r = 9$.
- Identify the TM mode with lowest cutoff frequency (i.e., specify the mn values for this TM_{mn} mode).
 - For this mode, find the cutoff frequency.
 - For a frequency 1.5 times cutoff, find the guide wavelength.
 - List all other modes (if any) with a cutoff frequency the same or lower than this mode. Do not actually compute these cutoff frequencies if you don’t have to!!

10. [4 pts.] Consider a cavity resonator with a conducting boundary. Assume the conducting walls are characterized by surface resistance R_s , and the dielectric (ϵ, μ) is low-loss with conductivity σ .
- Give the EXACT definition for Q (in general).
 - Write an explicit formula for Q . This formula should involve integrals of field quantities \vec{E}, \vec{H} (No other field quantities should appear!!). Use $\int_S dS$ to denote integration over the conducting boundary, and $\int_V dV$ to denote integration over the volume of the resonator. When doing the integral on the surface, you must show which components (i.e., tangential and/or normal) are involved.
 - You can use your formula for Q to obtain a formula for the $3dB$ bandwidth of the resonance; this formula should involve the integrals only, and should not (explicitly) involve the resonant frequency! Obtain this formula.
 - Even if you could not finish b,c, you can still answer this: is the formula for the $3dB$ bandwidth in part c an exact or approximate formula?
11. [5 pts.] Given the following scattering matrix of a 2-port:

$$S = \begin{bmatrix} 0.8 & -j0.4 \\ j0.4 & 0.9 \end{bmatrix}$$

- Compute the power dissipation matrix.
 - Is the network lossless?
 - Is the network reciprocal?
12. [4 pts.] A scattering matrix S is defined for an N -port relative to a reference impedance Z_0 . If a_i, b_i denote the incident and reflected waves at port i , and V_i, I_i the voltage and current at port i :
- Write the general relation for a_i, b_i in terms of V_i, I_i .
 - If port i is terminated in a load $Z_L = Z_0$, then **use your formulas** (not just something you may have memorized) to specify the condition imposed on a_i and/or b_i .
 - In general, the power flowing in at port i is $\frac{1}{2} \text{Re}(V_i I_i^*)$. Write this in terms of a_i, b_i instead.
13. [3 pts.] Let P_{diss} be the power dissipation matrix of an N -port. Specify the conditions on the eigenvalues for each of the following:
- passive
 - lossless
 - active

14. **[6 pts.]** Consider a lossless circulator. Assume “symmetry” in the sense that the return loss, isolation, etc. are the same regardless of which port is used as the input. Given that $|S_{12}| = 0.9$, and the return loss is $20dB$.
- Draw a symbol for the circulator, with the ports numbered.
 - Compute the magnitude of every scattering parameter (on a linear scale).
 - Compute the insertion loss, isolation and directivity, all in dB.
15. **[6 pts.]** Consider a directional coupler. Assume “symmetry,” for example the primary and secondary lines are actually interchangeable. Call 1 – 2 the primary line, and 3 – 4 the secondary line, with $1 \rightarrow 2$ and $3 \rightarrow 4$ considered “forward” directions.
- Each of the four quantities $|S_{i2}|$, $1 \leq i \leq 4$, expressed in a dB scale, has a “name.” For example, one of them is called the (through) insertion loss. Give the names, and identify each as $|S_{i2}|$
 - Using two of these four names, we can introduce a new quantity as _____ = _____ - _____ . Write this (in words).

16. [8 pts.] Refer to Figure 16. A three-port network, with ports labeled 1, 2, 3, respectively, is comprised of a tee (ports labeled 1A, 2A, 3A) with scattering matrix:

$$S_A = \begin{bmatrix} \frac{1}{2} & \frac{1}{2} & \frac{1}{\sqrt{2}} \\ \frac{1}{2} & \frac{1}{2} & -\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 \end{bmatrix}$$

and a directional coupler (ports labeled 1B, 2B, 3B, 4B) with:

$$S_B = \begin{bmatrix} 0 & \frac{1}{\sqrt{2}} & 0 & j\frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & 0 & -j\frac{1}{\sqrt{2}} & 0 \\ 0 & -j\frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} \\ j\frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} & 0 \end{bmatrix}$$

Port 3A of the tee is connected to port 1B of the coupler through a waveguide segment with $\lambda/4$ length. Port 2A of the tee is terminated in a short circuit, and port 4B of the coupler is terminated in a matched load. The resulting 3-port is determined by the associations $1 = 1A$, $2 = 2B$, $3 = 3B$.

GIVEN: (You do not have to check the following, but it is true): Both the tee and coupler are lossless.

DO NOT COMPUTE THE WHOLE SCATTERING MATRIX OF THE THREE PORT!!!! ONLY DO THE FOLLOWING!!!!

- By inspection (brief justification) determine if the overall three-port is: lossless, passive, reciprocal.
- Compute the scattering parameters (only): S_{11} , S_{12} and S_{32} . Compute these parameters directly, i.e., do not use reciprocity or other “tricks.” Give brief explanation of what you are doing, i.e., don’t just write down a final answer; even if correct, I may mark you wrong if I don’t see your work (e.g., if something turns out to be 0, you may have the right answer even if your method is wrong).